



# **TFAWS 2015**

Thermal Coatings Seminar Series Training Part 1: Properties of Thermal Coatings

NASA GSFC Contamination and Coatings Branch – Code 546 Hosted by: Jack Triolo - SGT, Inc.

August 6, 2015



### Agenda

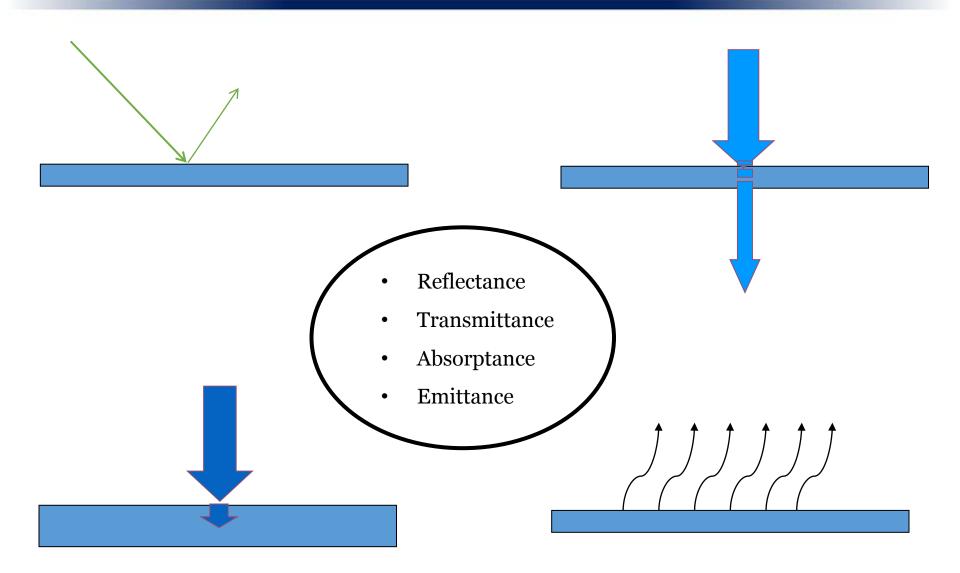


- The Relationship of Coating Properties That We Can "Easily" Measure vs. the Properties We Need... $\alpha_S$  &  $\epsilon_H$
- How Solar Absorptance is Determined
  - Description of Solar Reflectance measurement techniques
  - Typical data
- How Thermal Hemispherical Emittance is Determined
  - Conversion of normal emittance to hemispherical emittance
  - Emittance vs. temperature
  - Description of measurement techniques
  - Typical data
- Factors that Influence Thermal Radiative Properties
- BRDF Specular and Diffuse
- GSFC Instruments Overview
- Types of Coatings Used at GSFC



# Thermal Radiative Properties of Coatings







### Thermal Radiative Properties of Coatings

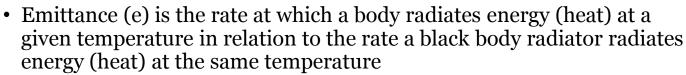


(Information Obtained From Thermal Radiative Properties Coatings, <u>Thermaphysical Properties of Matter</u>, Volume 9)

 Radiant energy is reflected, transmitted and/or absorbed by a surface or material

$$r + t + a = 1$$
, for materials, where  $t = 0$ ,  $r + a = 1$ , or  $a = 1 - r$ 

Where: Reflectance = r, Transmittance = t, and Absorptance = a

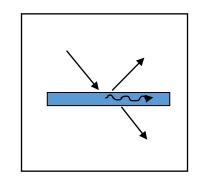


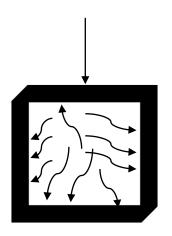


• Ideal radiator, when in thermal equilibrium, the body emits radiant energy at the same rate at which it absorbs

$$\alpha = e$$

• In the Aerospace Industry, a and e are never directly measured – THEY ARE CALCULATED!







## Solar Absorptance Property Measurement



- At GSFC, the instrumentation used to calculate the solar absorptance measures over the spectral range of 250 to 2800 nanometers (.25 to 2.8 microns). An integrating sphere is used to measure the coating's reflectance for the solar absorptance calculation
- Solar Absorptance is the total solar energy absorbed by the surface divided by the total solar energy integrated as a function of the wavelength

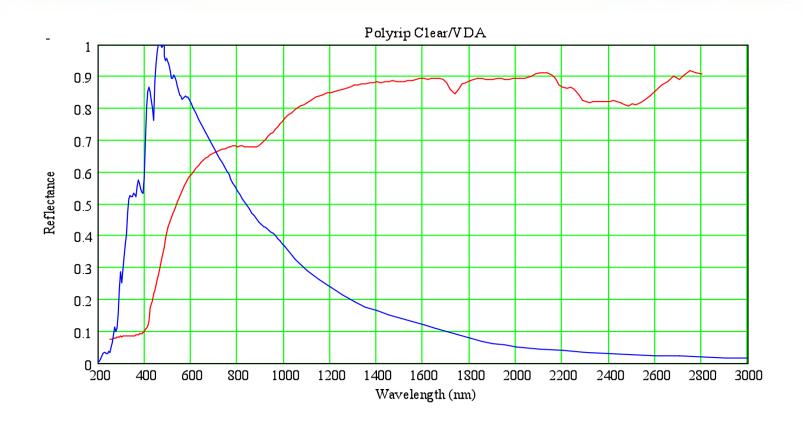
$$\alpha_{s} = 1 - \frac{\int_{250}^{2800} R(\lambda) \cdot S(\lambda) d\lambda}{\int_{250}^{2800} S(\lambda) d\lambda}$$

- Where R = reflectance, S = solar energy,  $a_s = solar absorptance$ , and l = wavelength
- The reflectance measurement is performed near-normal (angle of incidence =  $15^{\circ}$ ). This measurement is typically sufficient for most surfaces up to approximately  $45^{\circ}$
- Whereas, when measuring cylindrical surfaces, spherical surfaces or angle of incidence greater than 45°, variations in the angle of incidence will influence the solar absorptance value and must be measured
- Typically the Johnson curve is used to represent the total solar energy over the solar spectrum



#### Reflectance and the Johnson Curve



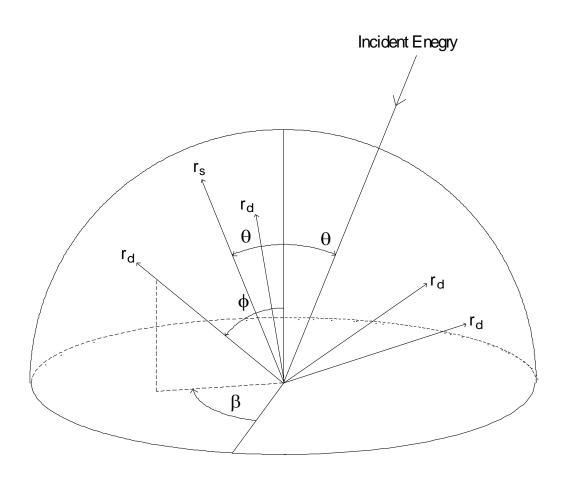


Johnson curve (blue) and the Polyrip clear/VDA (red) Solar Absorptance value = .405



# Directional Total Reflectivity



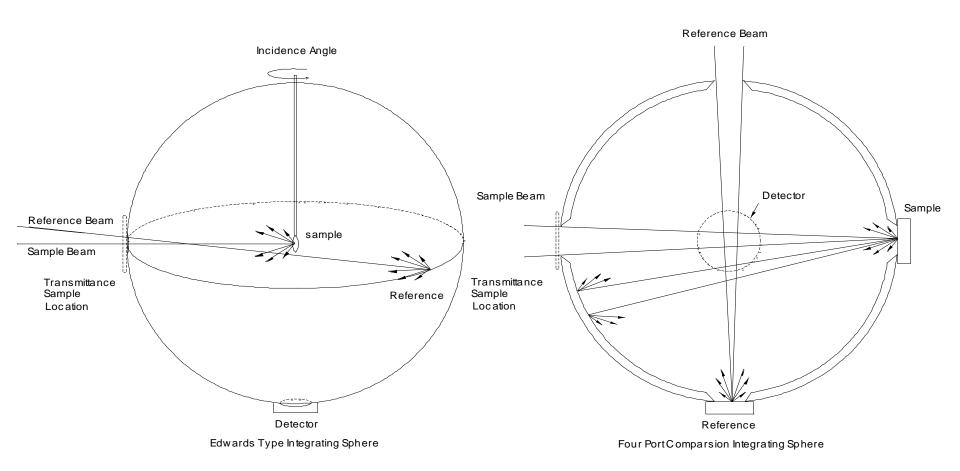




# Two Types of Integrating Spheres



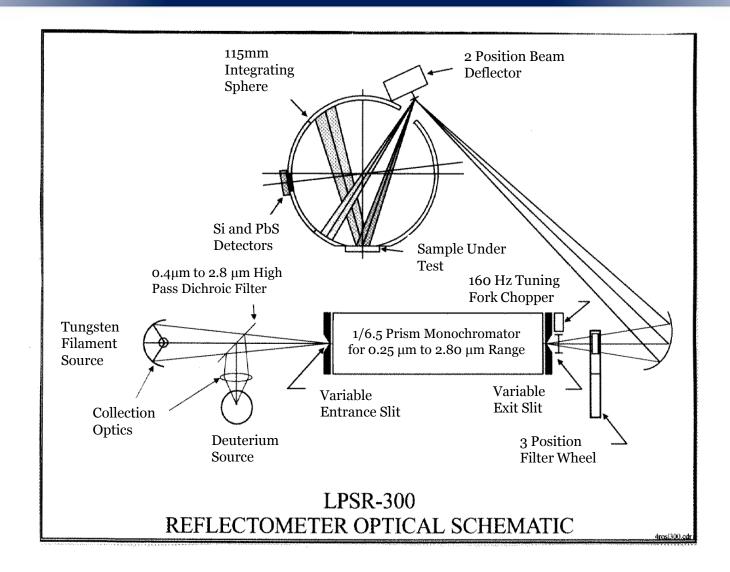
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#### LPSR-300 Reflectometer Optical Schematic

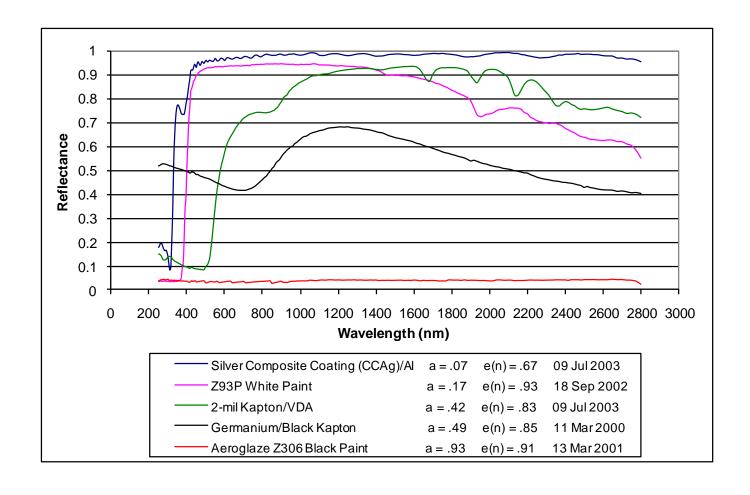






# Reflectance Curves of Various Thermal Coatings







#### **Emittance Property Calculation**



#### Normal Emittance

- At GSFC, the instrumentation used to calculate the normal reflectance measures over the spectral range of 5 to 100 microns at room temperature
- The normal emittance is calculated by measuring the reflectance of a material's surface in the infrared region of the spectrum and subtracting the measured reflectance from one (for opaque coatings only)

$$\varepsilon_N = 1 - \frac{\int_0^\infty R(\lambda)B(\lambda)d\lambda}{\int_0^\infty B(\lambda)d\lambda}$$

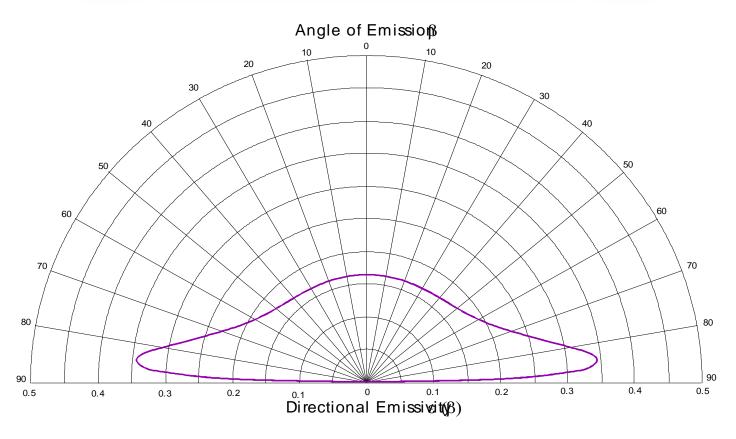
#### • Hemispherical Emittance

- For thermal modeling and analysis, the emittance must be in terms of a hemispherical (total body) emittance value. Converting normal emittance to hemispherical emittance can be accomplished by using a conversion table and chart by E. Schmidt, E. Eckert, and M. Jakob
- Hemispherical emittance can also be determined by calorimetric emittance measurement
- With the addition of an ellipsoidal attachment, GSFC also has the capability of calculating hemispherical emittance as a function of temperature by radiometric reflectance measurement



# Directional Emissivity Curve For a Conductor



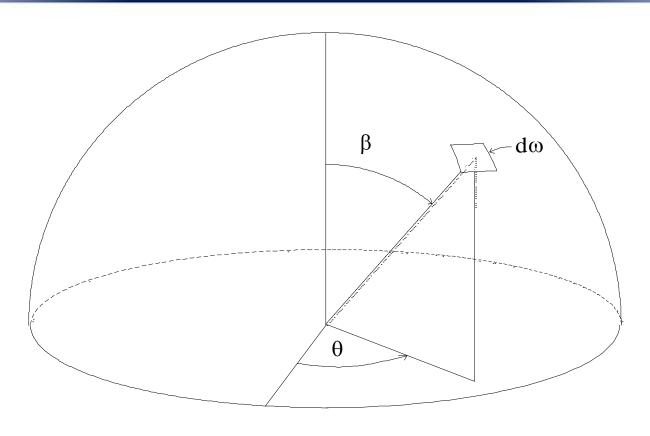


Directional emissivity curve for a conductor with an index of refraction of n = 5.7 + i9.7



# Hemispherical Emissivity Coordinate System





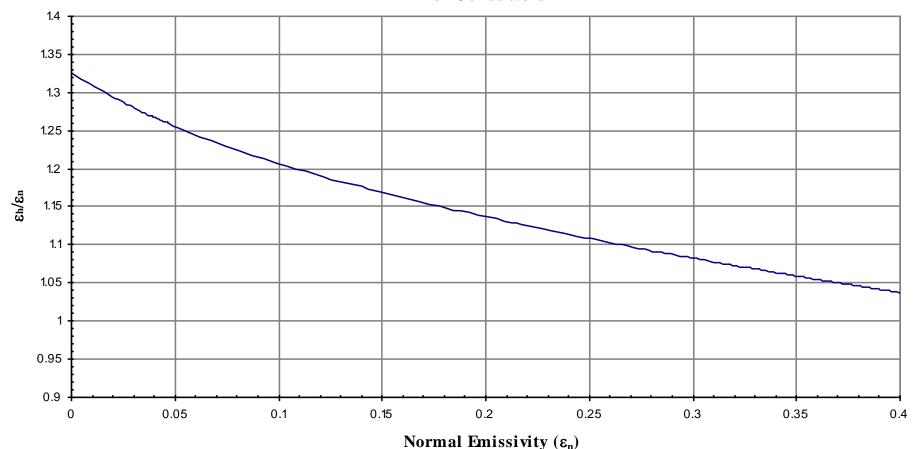
$$\varepsilon_{H} = \frac{1}{\pi} \int_{0}^{2\pi} \varepsilon(\beta, \theta, )\cos \beta d\omega$$



## Ratio of Hemispherical to Normal Emissivity for Conductors



#### Ratio of Hemispherical to Normal Emittance for Conductors





# Directional Emissivity Curve for a Dielectric



# Angle of Emissionβ 30 80 90 0.4 0.8 1.0 1.0 0.8 0.6 0.4 Directional Emissivity $\varepsilon$ ( $\beta$ )

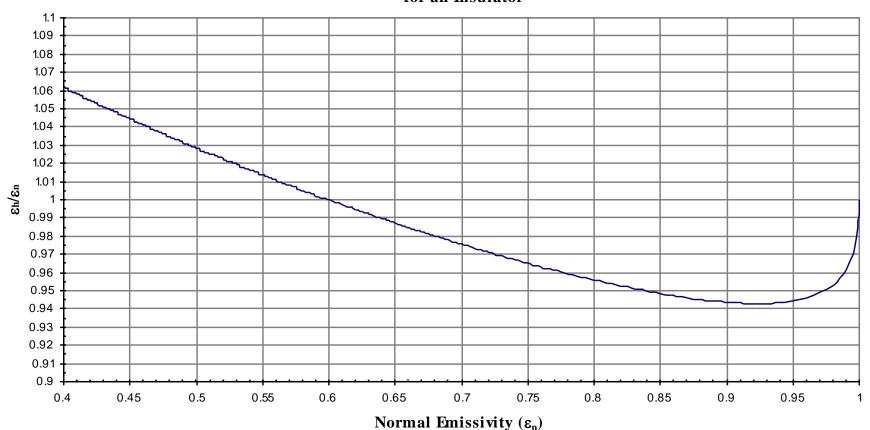
Directional emissivity curve for a dielectric with an index of refraction of n=1.5



# Ratio of Hemispherical to Normal Emissivity for Insulators



# Ratio of Hemispherical to Normal Emittance for an Insulator





## DB 100 Optical Diagram





Illumination: Hemispherical

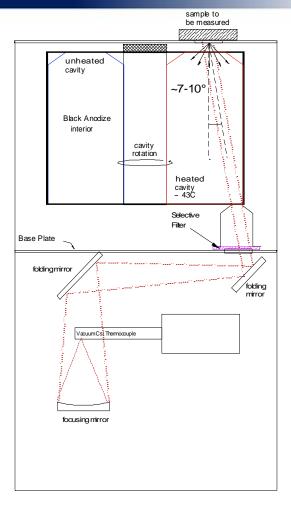
Detector: Directional ~7-10 deg

Detector type: CsI vacuum thermocouple

Detector Range: 5?-40µm?

Accuracy:  $\pm 0.02$  sample must be gray

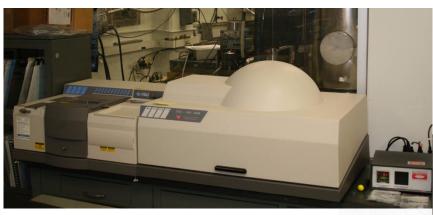
Measurement: Hemispherical-Directional Reflectance





# SOC 100 Optics





Illumination: Hemispherical

Detector: 10°-80°

Detector type: FTIR: Si, KBr, Pe

Detector Range: 2-100µm

Accuracy:  $\pm$ ?

Measurement: Hemispherical-Directional

Spectral

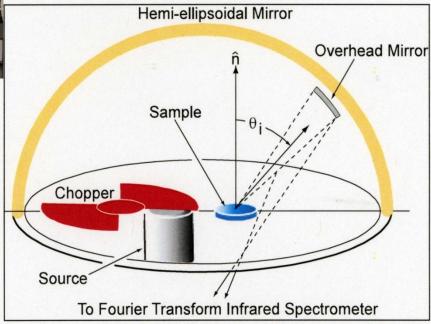


Figure 19: SOC-100 HDR Internal Layout.



# Temp200A Optical Diagram





Illumination: 15°

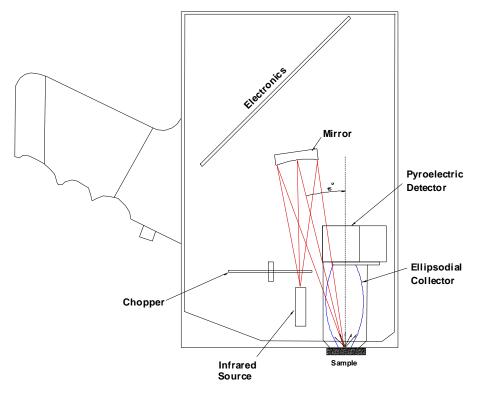
Detector: Hemispherical Detector type: Pyroelectric

Detector Range: 3-35µm

Accuracy:  $\pm 0.01$  for gray samples

 $\pm 0.03$  for non-gray samples

Measurement: Directional-Hemispherical Reflectance

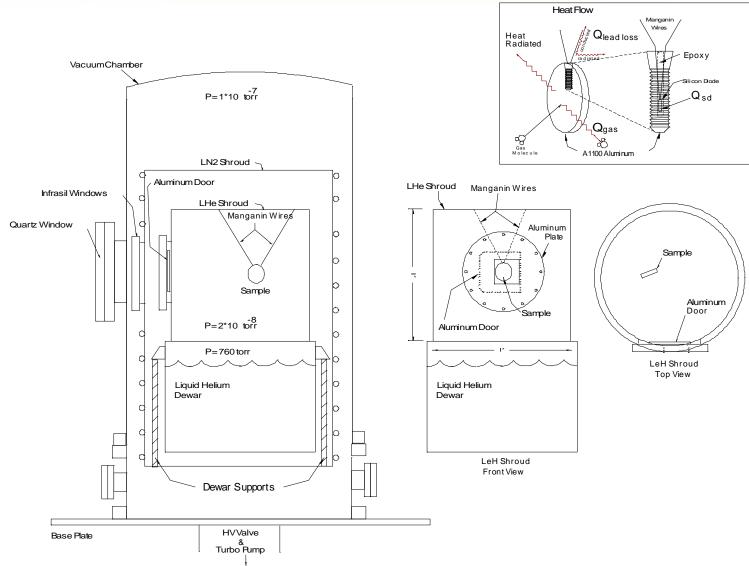


Temp 2000A Optical System



# Emittance by the Calorimetric Technique





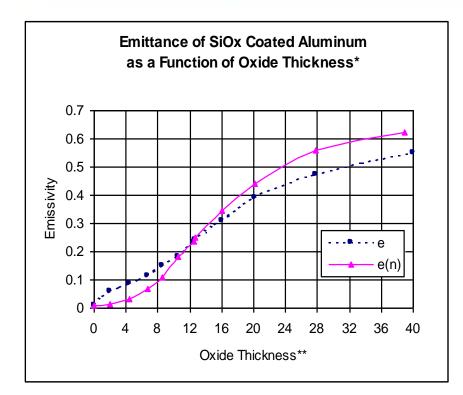
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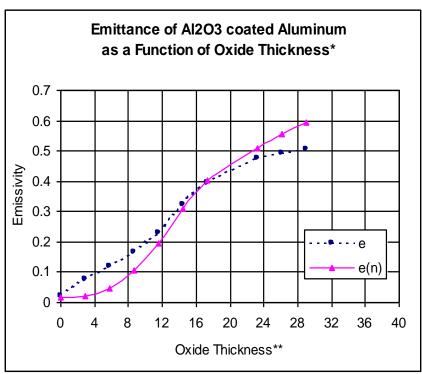
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#### Dielectrics over Metals







- \* Charts reproduced from Heaney, Triolo, and Hass, "Evaporated Thin Films For Spacecraft Temperature Control Applications", July 1977.
- \*\* Oxide Thickness is represented as  $\lambda/4$  at 550 nm.



# Spectral Reflectance



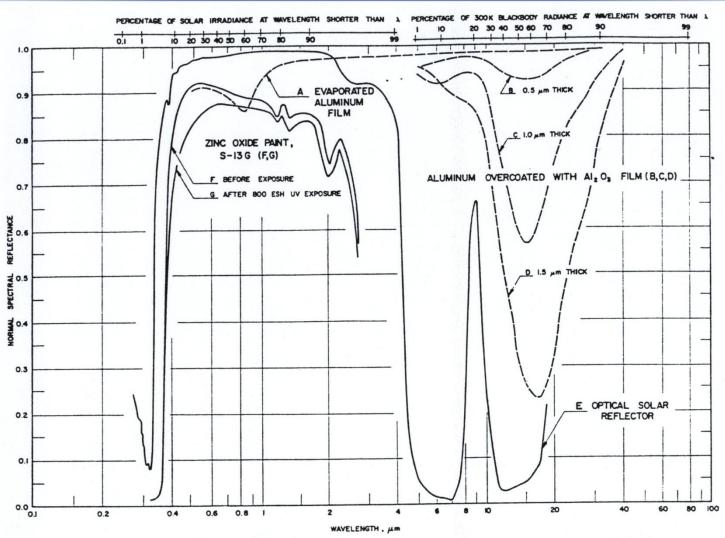


Fig. 7. Typical spectral characteristics of selected coatings: A, evaporated aluminum, B, C, and D, evaporated aluminum over-



# Blackbody Spectral Radiance



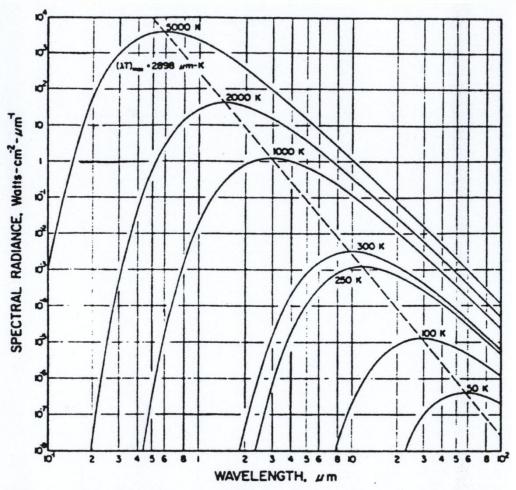
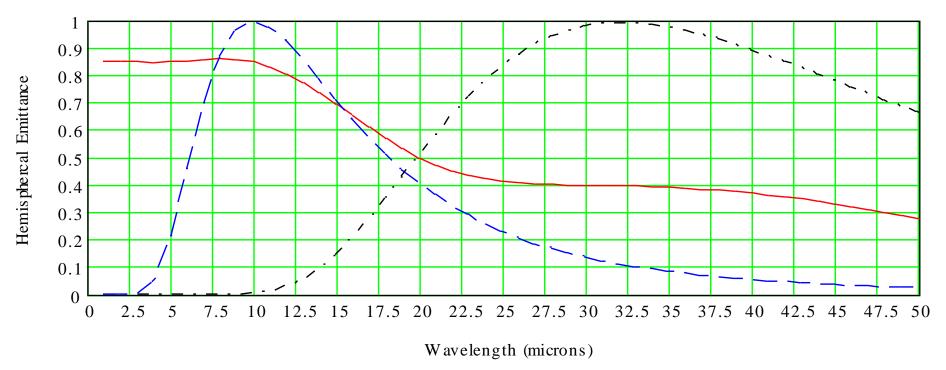


Fig. 1. The Planck distribution law, spectral radiance of blackbody radiation as a function of temperature and wavelength.



# Emittance of a Hypothetical Coating and Two Black Body Temperature Curves





—— Emittan ce of Coatin g

— · Black Body 290° K

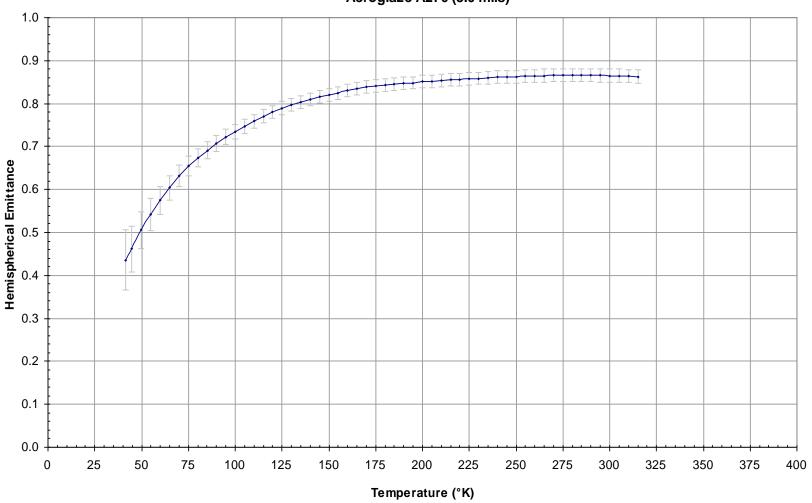
− · · Black Body 90° K



# Calorimetric Results for A276



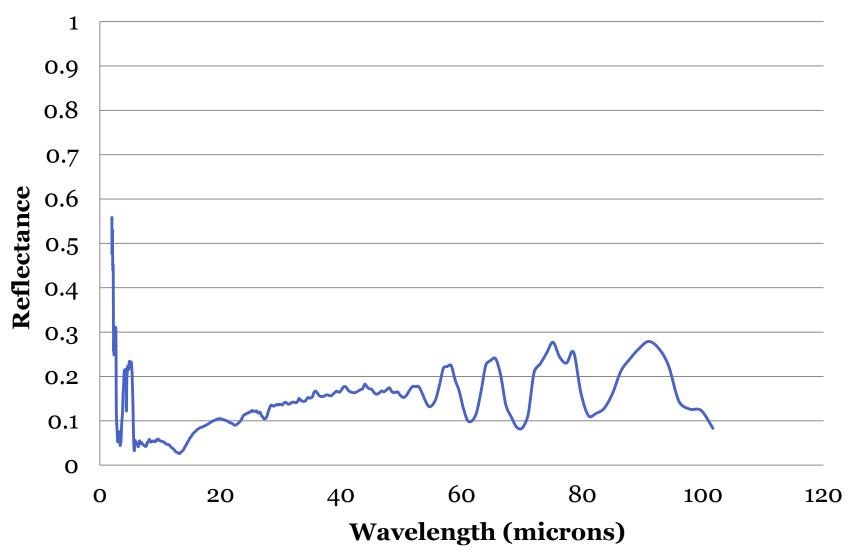






# Infrared Reflectance of A276







#### Factors that Influence Thermal Radiative Properties

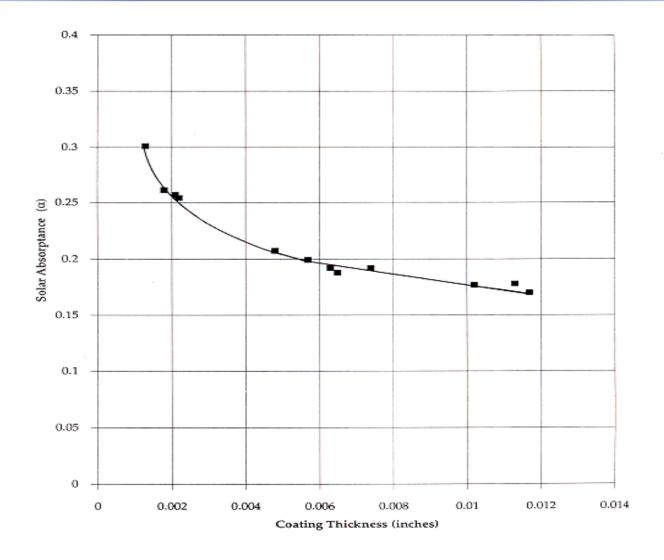


- Solar Absorptance and/or Emittance Values Influencing Factors:
  - Surface Finishes
    - Highly Polished (mirror-like/optical surface)
    - Polished
    - Buffed
    - Matt
    - Machined
  - Substrate Texture
    - Rough versus Smooth
    - Woven
    - Bead Blasted (sand, glass, etc...)
  - Immersion Rate for Chemical Coatings Processes (i.e., Anodized, Irridited)
  - Coating Thickness
  - Coating Adherence
  - Transmissivity
  - Electrical Conductivity
  - Contaminants
  - Sample/Hardware Size and Configuration



# Solar Absorptance of a White Silicone Paint as a Function of Thickness







#### NASA-GSFC Thermal Control Coatings Measurement Instrumentation



- AZTek Laboratory Portable Spectroreflectometer (LPSR-300 and LPSR-200)
- Cary 500 IR/Vis/UV Spectroreflectometer
- Geir-Dunkle DB-100 Reflectometer
- SOC-100 Infrared Spectroreflectometer (2μ 100μ)
- Bi-Directional Reflectance Distribution Function (BRDF)
- Light Analyzer Microscopic Imager
- Calorimetric Emittance Chamber





# Bi-directional Reflectance Distribution Function

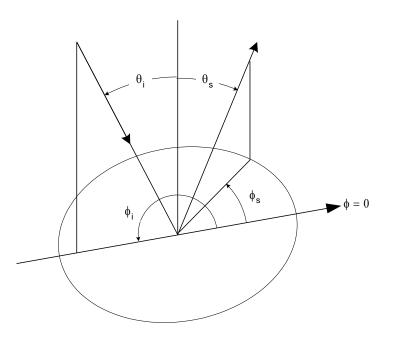


• BRDF is a precise measurement of the intensity and direction of the reflection of light from a surface

Power reflected per unit area per solid angle Power arriving per unit area  $\mathbf{X} \cos(\theta_s)$ 

• BRDF is a point property of a surface. BRDF is a function of the direction of the incident light and the direction of the scattered light

• Our facility has the capability to measure light scattering at 632.8 nm, 442 nm, and 830 nm





#### Bi-directional Reflectance Distribution Function



Perfectly diffuse or lambertian surface has constant BRDF;

Power reflected per unit area per solid angle = BRDF X power arriving per unit area  $X cos(\theta_s)$ 

- BRDF measurements/data are used to:
  - Calculate the amount of light or energy scattered by specific surfaces in critical applications
    - Example -- sunshield
  - Evaluate or monitor the condition of a surface with respect to contamination or roughness
    - Example -- optics (mirrors)
  - Determines specularity of surfaces for special cases
  - Calculate solar pressure



# Types of Thermal Control Coatings



- **Paints** (Z93P, Z306, AZ93, Z93-C55, AZWLA2, Z276, Z307, etc....)
- Metals (Al, Ag, Au, Ni, Stainless Steel, Cu, Mg, Ti, etc...)
- Sheet Films (Kapton®, Ge/Black Kapton®, Black Kapton®, Teflon (FEP), etc...)
- **Tapes** (Ag/FEP, Al/FEP, Al/Kapton®, Al Foil, Kapton®, Black Kapton® etc...)
- Vacuum Deposited Coatings [Evaporated/Sputtered]
  - **Metals** (Al, Ag, Au, Ti, Ge, Cr, Ni, etc...)
  - **Dielectrics** (Al<sub>2</sub>O<sub>3</sub>, SiO<sub>x</sub>, CCAg, CCAl, Dark Mirror, etc...)
- Conductive Coatings (ITO, ATO, Ge, Z93-C55, Z307, etc...)
- Anodized Aluminum (Black, Hard, Clear, Plain, etc...)
- Chemical Conversion (Irridite, Alodine, etc...)
- Optical Surface Reflectors [OSR]
- Solar Cells



#### References



- "Thermal Radiative Properties Coatings", Y.S. Touloukian, D. P. DeWitt, R. S. Hernicz; Thermophysical Properties of Matter, Volume 9; Pages 1a 50a, IFI/Plenum, New York-Washington, 1972, (Introduction to Volumes 7, 8 and 9).
- "Spacecraft Thermal Control Coatings References", NASA/TP-2005-212792, by Lonny Kauder, December 2005.